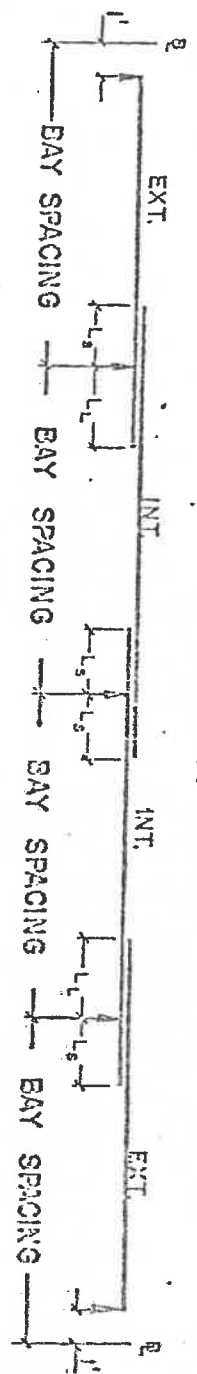




LOAD =  $N-2520 + 3PST$  CONTINUOUS PURLIN LOAD CHART  
 Purlins =  $4'-6''$  o/c  
 $4.5' \times 30 PST = 135.0 PLF$  4 - SPAN

$L_0$  = Short Lap  
 $L_c$  = Long Lap  
 $F_b = 0.6(F_y) = 0.6(50) = 30 \text{ ksi}$



PURLIN EXT GA	INT GA	$L_0 = 1'-0''$					$L_0 = 2'-0''$					$L_0 = 3'-0''$					$L_0 = 4'-0''$				
		14'	15'	17'	18'	19'	21'	22'	23'	24'	25'	26'	27'	28'	29'	30'	31'	32'	33'	34'	
16	16	457	331	281	242	210	189	168	149	134	121	120	110	101	93	85					
15	16	511	377	320	276	240	213	192	171	153	138	135	125	115	106	97					
14	16	546	417	363	321	271	239	216	194	174	156	152	140	129	120	110					
13	16	511	467	414	369	330	268	244	224	202	178	174	160	142	128	116					
12	16	673	515	443	381	331	296	269	232	203	179	181	161	143	129	116					
13	15	642	491	435	378	329	281	256	235	211	190	182	169	156	144	130					
12	15	706	540	478	427	376	310	283	259	229	202	201	181	162	145	131					
11	15	750	582	502	432	375	338	305	263	230	203	206	192	163	146	132					
12	14	741	566	501	443	386	324	296	271	248	223	210	195	181	162	147					
11	14	750*	583*	519*	465*	419*	353	322	295	258	227	229	204	182	164	148					
11	13	752*	584*	520*	467*	421*	380	346	316	283	255	246	227	210	195	177					

\* Denotes systems controlled by connection  
 Allowable load per foot is the total allowable (dead + live) and is based on an analysis of the system considering the increased stiffness over the support and the connection capacities at the supports with the allowable bending stress set at 30 ksi for all systems.

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Simple Span 9.5 Z LIGHT GAGE BEAMS

TOTAL ALLOWABLE LOAD PER FOOT (W<sub>T</sub>)

SPAN (L)	8.5 Z 16			8.5 Z 15			8.5 Z 14			8.5 Z 13			8.5 Z 12			8.5 Z 11		
	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ	F <sub>b</sub> =30 F <sub>b</sub> =40	F <sub>b</sub> =30 F <sub>b</sub> =40	Δ
10	422	562	791	177	637	889	538	717	1001	650	966	1208	762	1015	1415	874	1165	1623
11	348	465	594	395	526	668	444	592	752	537	716	907	629	839	1063	722	963	1220
12	293	399	498	331	442	514	373	498	579	451	601	699	529	705	819	606	809	939
13	249	332	360	292	377	405	318	424	455	364	512	550	450	601	644	517	669	739
14	215	267	288	243	325	324	274	365	364	331	442	440	398	519	515	445	594	591
15	187	250	234	212	283	263	239	318	296	288	385	358	338	451	419	388	517	481
16	164	219	193	186	248	217	210	280	244	253	338	295	297	396	345	341	455	395
17	145	194	161	165	220	181	186	248	203	224	299	245	263	351	288	302	403	330
18	130	173	135	147	196	152	166	221	171	200	267	207	235	313	242	269	359	278
19	116	155	115	132	175	129	149	198	145	180	240	176	211	281	206	242	322	236
20	105	140	98	119	159	111	134	179	125	162	216	151	190	253	176	218	291	202
21	95	127	85	108	144	96	121	162	108	147	196	130	172	230	152	198	264	175
22	87	116	74	93	131	83	111	148	94	134	179	113	157	132	132	180	240	152
23	79	106	65	90	120	73	101	135	82	122	163	99	144	116	165	165	220	133
24	73	97	57	82	110	64	93	124	72	112	150	87	132	102	116	151	202	117
25	67	90	50	76	101	56	86	114	64	104	138	77	121	90	139	186	186	103
26	62	83	45	70	94	50	79	106	56	96	128	68	112	80	129	172	172	92
27	57	77	40	65	87	45	73	98	50	89	118	61	104	71	119	159	159	82
28	53	71	35	60	81	40	68	91	45	82	110	55	97	64	111	148	148	73
29	50	66	32	56	75	36	63	85	41	77	103	49	90	58	103	138	138	66
30	45	62	29	53	70	32	59	79	37	72	96	44	84	52	97	129	129	60

S<sub>x</sub> = 2.11

S<sub>x</sub> = 2.39

S<sub>x</sub> = 2.69

S<sub>x</sub> = 3.23

S<sub>x</sub> = 3.01

S<sub>x</sub> = 4.37

24'-0" EAVE

LOAD

DEFLECTION

M = F<sub>s</sub> S<sub>x</sub> =  $\frac{W(L)(12)}{2}$

Δ = L/180 =  $\frac{S W L^4}{504 E I}$

17'-4" Avg. Space = 5.84' x 20PSF = 116.8 PLF  
 12'-4" Avg. = 5.0' x 20PSF = 100 PLF  
 7'-4" Avg. = 6.3' x 20PSF = 126.0 PLF

W =  $\frac{F_s S_x (2)}{L^2 (12)}$

Δ =  $\frac{(504) E I}{100 (S) L^3}$

5.4	1 (in) <sup>4</sup>
15	9.05
15	10.17
14	11.44
13	13.51
12	16.18
11	19.56

E = 29500ksi

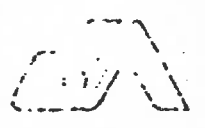
Section Properties  
8.5" - Light Gage Z Shapes

Section	Lip Angle	Theoretical		Thick (In)	Radius of Bend	Gage	Full Area (In) <sup>2</sup>	Eff Sx (In) <sup>3</sup>	Full Sx (In) <sup>3</sup>	Full Ix (In) <sup>4</sup>	Rx (In)	Full Sy (In) <sup>3</sup>	Full Iy (In) <sup>4</sup>	ry (In)
		Lip Depth	Lip Depth											
8.5Z16	45	0.61"	0.060	0.060	0.3125	16	0.85	2.11	2.13	9.05	3.26	0.38	1.09	1.13
8.5Z15	45	0.56"	0.067	0.067	0.3125	15	0.96	2.39	2.39	10.17	3.26	0.43	1.27	1.15
8.5Z14	45	0.71"	0.075	0.075	0.3125	14	1.08	2.69	2.69	11.44	3.26	0.50	1.42	1.17
8.5Z13	45	0.79"	0.090	0.090	0.3125	13	1.30	3.25	3.25	13.81	3.25	0.62	1.87	1.20
8.5Z12	45	0.85"	0.105	0.105	0.3125	12	1.53	3.81	3.81	16.18	3.25	0.75	2.29	1.22
8.5Z11	45	0.93"	0.12"	0.12"	0.3125	11	1.76	4.37	4.37	18.56	3.25	0.88	2.75	1.25

8.5" - Light Gage C Shapes

Section	Lip Angle	Theoretical		Thick (In)	Radius of Bend	Gage	Full Area (In) <sup>2</sup>	Eff Sx (In) <sup>3</sup>	Full Sx (In) <sup>3</sup>	Full Ix (In) <sup>4</sup>	Rx (In)	Full Sy (In) <sup>3</sup>	Full Iy (In) <sup>4</sup>	ry (In)
		Lip Depth	Lip Depth											
8.5C16	90	0.54"	0.060	0.060	0.0938	16	0.85	2.03	2.11	8.95	3.25	0.33	0.62	0.26
8.5C15	90	0.58"	0.067	0.067	0.0938	15	0.95	2.34	2.36	10.02	3.25	0.38	0.71	0.26
8.5C14	90	0.62"	0.095	0.095	0.0938	14	1.07	2.64	2.64	11.24	3.25	0.43	0.80	0.27
8.5C13	90	0.70"	0.090	0.090	0.0938	13	1.29	3.19	3.18	13.52	3.24	0.53	0.99	0.28
8.5C12	90	0.71"	0.105	0.105	0.1275	12	1.48	3.61	3.61	15.33	3.22	0.59	1.10	0.28
8.5C11	90	0.77"	0.120	0.120	0.1875	11	1.70	4.12	4.12	17.51	3.21	0.69	1.28	0.27

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No. \_\_\_\_\_ Roof Framing  
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 Date 12/1/73  
 Prepared by \_\_\_\_\_  
 Reviewed by \_\_\_\_\_